



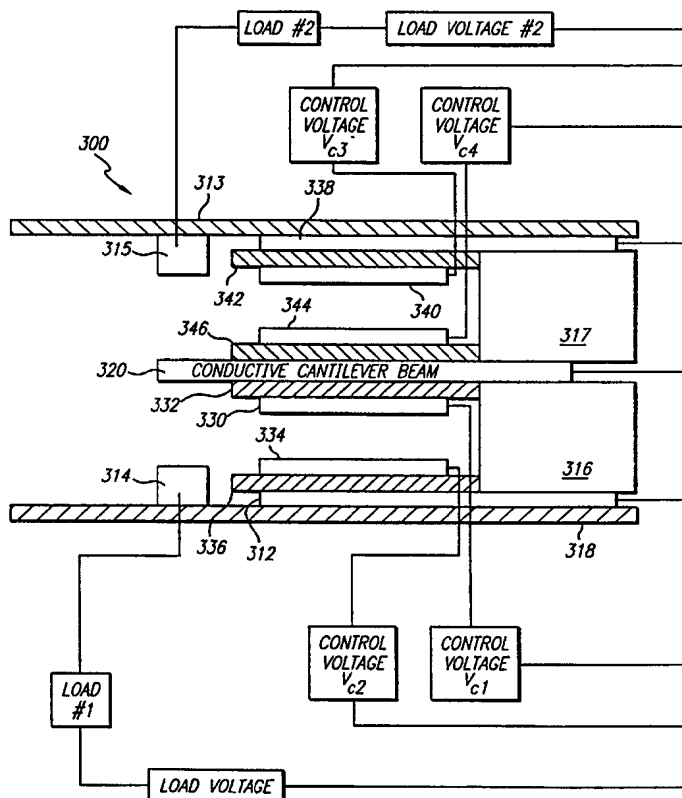
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(54) Title: METHOD AND APPARATUS FOR AN IMPROVED SINGLE POLE DOUBLE THROW MICRO-ELECTRICAL MECHANICAL SWITCH

## (57) Abstract

A single pole, double throw micro-electromechanical (MEM) switch. The inventive switch includes a first contact providing a first terminal of the switch. A second contact provides a second terminal of said switch. A cantilever beam provides a third terminal of the switch. The inventive switch includes a system for electrostatically pushing or pulling the beam to disengage the first contact and engage the second contact. In an illustrative implementation, the system for electrostatically operating the switch includes a first charge storage structure on the beam, a second charge storage structure on the switch, and an electrical supply for creating an electrical charge on the first and the second charge storage structures. The first and second charge storage structures are effective to create a force of repulsion therebetween on the application of an electrical charge thereto. The "pull" electrostatic force closes the MEM switch. The "push" force aids in opening the switch. The "push" capability is the result of the use of like (same polarity) electrostatic charges on the control surfaces. The like charges provide an electrostatic repulsion force during the switch opening process.



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## **METHOD AND APPARATUS FOR AN IMPROVED SINGLE POLE DOUBLE THROW MICRO-ELECTRICAL MECHANICAL SWITCH**

### **BACKGROUND OF THE INVENTION**

#### Field of the Invention

The present invention relates to electrical and electronic circuits and components. More specifically, the present invention relates to micro-electromechanical (MEM) switches.

#### Description of the Related Art

An electrostatic MEM switch is a switch operated by an electrostatic charge and manufactured using micro-electromechanical techniques. A MEM switch may control electrical, mechanical, or optical signal flow. Current MEM switches are usually single pole, single throw (SPST) configurations having a rest state that is normally open. Application of an electrostatic charge to the control electrode (or opposite polarity electrostatic charges to a two-electrode design) will create an attractive electrostatic force ("pull") on the switch causing the switch to close. Currently, the switch opens by removal of the electrostatic charge on the control electrode(s), allowing the mechanical spring restoration force of the armature to open the switch.

Unfortunately, electrostatically actuated MEM switches constructed in accordance with conventional teachings typically close faster than they open and often suffer "stiction" effects that hinder the opening process or cause the switch to fail closed. Hence, the opening and closing ("transition speed") of conventional MEM switches has some limitations.

For many current applications, there was a need to increase the transition speed of a MEM switch. U. S. Patent Application no. 09/198,669, filed November 23, 1998, by the present Applicants (R. D. Streeter *et al.*) and entitled METHOD AND APPARATUS FOR AN IMPROVED MICRO-ELECTRICAL MECHANICAL SWITCH (Atty. Docket No. PD 970596), the teachings of which are incorporated herein by reference, addresses the need in the art for a MEM switch having an improved transition speed. However, the switch disclosed by Streeter *et al.* is a single pole, single throw switch.

For certain current applications, there is a need for a single pole, double throw MEM switch having a high transition speed. Hence, a need remains in the art for further improvements in MEM switches.

## SUMMARY OF THE INVENTION

The need in the art is addressed by the single pole, double throw MEM design and method of the present invention. The inventive switch includes a first contact providing a first terminal of the switch. A second contact provides a second terminal of said switch. A cantilever beam provides a third terminal of the switch. The inventive switch includes a system for electrostatically pushing the beam to disengage the first contact and engage the second contact.

In an illustrative implementation, the system for electrostatically operating the switch includes a first charge storage structure on the beam, a second charge storage structure on the switch, and an electrical supply for creating an electrical potential  
5 between the first and the second charge storage structures. The first and second charge storage structures are effective to create a force of repulsion therebetween on the application of an electrical potential thereto.

The “pull” electrostatic force closes the MEM switch. The “push” force aids in opening the switch. The “push” capability is the result of employing like (same  
10 polarity) electrostatic charges on the control surfaces. The like charges achieve an electrostatic repulsion force during the switch opening process.

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## BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a diagram of a conventional micro-electromechanical (MEM) switch.

Fig. 2 is a schematic diagram of a typical setup using a conventional MEM  
20 switch.

Fig. 3 is a sketch of the control voltage applied to a conventional MEM switch illustrating optimum driving waveform for MEM switch closure.

Fig. 4 is a waveform for enhanced conventional MEM switch opening.

Fig. 5 is a diagram of an improved MEM switch constructed in accordance  
25 with the teachings of the above-referenced Streeter application.

Fig. 6 is a schematic diagram of an electrical circuit using the improved MEM switch of the above-referenced Streeter application.

Fig. 7 illustrates exemplary waveforms for driving the improved MEM switch of the above-referenced Streeter application.

Fig. 8 is a diagram of the single pole, double throw MEM switch of the present invention.

Fig. 9 is a diagram of an alternative embodiment of the single pole, double throw MEM switch of the present invention without isolation between the switched  
5 signal and the control signal.

Fig. 10 is a diagram of a second alternative embodiment of the single pole, double throw MEM switch of the present invention with isolation between the switched signal and the control signal.

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## DESCRIPTION OF THE INVENTION

Illustrative embodiments and exemplary applications will now be described  
15 with reference to the accompanying drawings to disclose the advantageous teachings of the present invention.

While the present invention is described herein with reference to illustrative embodiments for particular applications, it should be understood that the invention is not limited thereto. Those having ordinary skill in the art and access to the teachings  
20 provided herein will recognize additional modifications, applications, and embodiments within the scope thereof and additional fields in which the present invention would be of significant utility.

Fig. 1 is a diagram of a conventional micro-electromechanical (MEM) switch. The switch 10' has an insulating support substrate 12' which serves as a base. A  
25 conductive contact 14' is mounted on one side of the substrate and a cantilever support 16' is mounted on the other. The cantilever support 16' supports a conductive cantilever beam 20'. A conductive control surface 18' is mounted on the substrate 12' between the conductive contact 14' and the cantilever support 16'.

The switch 10' is shown as a normally open (NO) switch contact structure. The open gap between the conductive contact 14' and the cantilever beam 20' is usually a few microns (1/1,000,000 meter) wide. When the switch closes, the cantilever beam 20' is in direct electrical contact with the conductive contact 14'.

5 A slightly larger gap exists between the cantilever beam 20' and the conductive control surface 18'. The larger gap keeps the conductive control surface from contacting the cantilever beam in normal operation. The total device is usually less than 1 mm in length, width and height. If the far end (the unattached end) of the cantilever beam is deflected toward the conductive contact, the cantilever beam will  
10 make ohmic contact with the conductive contact and be physically stopped by the contact. The cantilever beam will not make electrical or physical contact with the control surface unless the beam is physically forced to make contact with the control surface.

In normal operation, the MEM switch 10' is drawn closed by placing an  
15 electric charge on the conductive control surface 18'. An opposite polarity charge is induced on the inner surface of the conductive cantilever beam 20' opposite to the control surface. This electric charge pair induces an electrostatic (coulomb) attractive force between the two surfaces. If the coulomb force is strong enough to overcome the spring restorative force of the cantilever beam, the coulomb force will deflect the  
20 beam toward the control surface and the conductive contact. This will close the switch. The potential between control surface 18' and the rest of the MEM switch determines the charge pair in accordance with  $Q = CV$ .

Fig. 2 is a schematic diagram of a typical setup using a conventional MEM switch. Those skilled in the art will appreciate that numerous circuit configurations are  
25 permitted using MEM switches. In Fig. 2, a control voltage supply 22' provides a control voltage  $V_c$  to the control surface 18'. The control voltage  $V_c$  induces a charge on the control surface in accordance with the relation  $Q = CV$ , where  $Q$  is the charge,  $C$  is the capacitance between the control surface and the cantilever beam, and  $V$  is the applied control voltage  $V_c$ . The load voltage  $V_l$ , supplied by a load voltage supply

24', allows current to flow through the load (delivering power to the load) when the MEM switch closes.

The cantilever beam restorative force is linearly proportional to the displacement from the rest position of the beam. A small coulomb force will make a small deflection of the beam, but will not cause the beam to fully deflect to the conductive contact. As the coulomb force raises by increasing the electric charge on the control surface, the beam deflection will increase. Additionally, the coulomb force is inversely proportional to the square of the separation distance between the charges. Thus, as the coulomb force draws the beam closer to the contact, the distance between the charged surfaces will decrease. This decreased distance between the charges will increase the coulomb force on a square-law basis without a proportional increase in the electric charge stored on the control surface. This action identifies a minimum switching voltage on the control surface that results in a continuous net attraction of the cantilever beam toward the control surface. Additionally, since the coulomb force (above the minimum required) is increasing on a square law basis while the cantilever spring restorative force opposing the coulomb force is only increasing linearly, the cantilever beam experiences a continuously increasing acceleration as it approaches the control surface and the conductive contact.

As long as the coulomb force exceeds the spring restorative force at every point in the deflection of the beam, the MEM switch will continue to close, and the beam will accelerate as it approaches the conductive contact.

It should be obvious that the maximum coulomb force exists as the cantilever beam touches the conductive contact and is at its closest approach to the control surface. The switch will be held closed by this maximum force. It should also be apparent that there is a maximum coulomb charge that can be applied to the control surface. An excess charge may result in an arc if the dielectric electric withstanding field strength (between the control surface and any other MEM switch structure) is exceeded or in an excess deflection of the cantilever beam causing it to touch the



control surface. Either of these actions will result in a discharge of the electrostatic charge and the elimination of the coulomb force holding the MEM switch closed.

The application of a fixed direct current (D.C.) voltage  $V_c$  to the control surface is the simple case of the control waveform driving the MEM switch to the closed position. The voltage  $V_c$  may be of either polarity, although the physical structure and the materials used in fabrication of the MEM switch may favor one polarity over the other. The application of the voltage to the control surface in the circuit of Fig. 2 will cause a charging current to flow briefly in the control circuit (consisting of the control surface 18', the beam 20' and the control voltage supply 22'). This charging current can be thought of as charging the capacitor formed by the control surface and the cantilever beam. The control voltage  $V_c$  must be above the minimum for switch closure and below the maximum (to prevent arcing), for the physical structure of the MEM switch, if proper operation is to occur.

Ideally, when the control surface is charged, the voltage  $V_c$  may be removed. This is usually not done due to leakage effects in the MEM switch and the changes that occur during switch closure.

It is also possible to reverse the control polarity while the switch is held closed so long as the time needed to discharge and recharge the control surface with the opposite polarity charge is much less than the time required for the cantilever beam to move sufficiently to disconnect the load circuit. The use of polarity reversal drive can create a mechanical wiping action on the load circuit contacts while the switch is closed and may be a benefit for certain contact metallurgy. Polarity reversal may also be useful in association with certain MEM fabrication methods.

The speed of switch closure can be controlled to some degree by controlling the magnitude of the charge on the control surface. The initial charge placed on the control surface will have a maximum value set primarily by arc limitations between the control surface and the remaining elements of the MEM switch. This maximum charge will apply a maximum coulomb force to the cantilever beam, resulting in a maximum initial closure rate for the beam. As the beam approaches the control surface during

closure, the capacitance will increase. While application of a constant voltage will result in an increase in the surface charge (through  $Q=CV$ ) and a resultant increase in the coulomb force beyond the square-law effect, the voltage may exceed the capabilities of the beam to control surface spacing. Thus, it may be necessary to  
5 reduce the control voltage as the switch closes to prevent a discharge arc of the stored charge. This leads to a decayed voltage waveshape versus time for the fastest MEM switch closure operation. The shape of the control voltage decay for the fastest closure depends on the constructional details of the MEM switch. When the MEM switch achieves closure, the control voltage must remain between the maximum closed  
10 voltage (determined by arc or cantilever deflection) and the minimum voltage needed to provide sufficient coulomb force needed to overcome the cantilever spring restoration force.

Fig. 3 is a sketch of the control voltage applied to a conventional MEM switch illustrating optimum driving waveform for MEM switch closure. The opening of a  
15 conventional MEM switch depends exclusively on the spring restoration force in the cantilever beam. Since the coulomb force holding the switch closed is stronger than the spring restoration force, the coulomb force must be reduced to a value as close to zero as possible to allow a maximum of opening force from the cantilever beam spring effect. The opening force may also need to overcome "stiction" effects resulting from  
20 the Casimir effect or from minor contact adhesion effects. While the control surface charge can be allowed to leak off slowly, this will delay the opening of the MEM switch. The opening speed can be improved by accelerating the discharge of the control surface charge. The proper selection of control voltage waveform can speed the opening process.

25 The conventional method to open the MEM switch 10' is to force the control surface voltage (relative to the cantilever beam) to zero volts through a low impedance source. A short circuit between the control surface and the cantilever beam is the optimum means of swiftly reducing the control voltage to zero. The electrical effect is

to rapidly discharge the capacitor formed by the control surface and the inner surface of the cantilever beam.

A method to further enhance the discharge of the control surface charge is to supply an opposite charge burst prior to driving the control surface voltage to zero.

5 The waveform to accomplish this is shown in Fig. 4.

Fig. 4 is a waveform for enhanced conventional MEM switch opening. However, this method does have some inherent limitations in that inserting less than the correct opposite charge will not provide the best reduction of coulomb force. Even worse, inserting an excess opposite charge will simply recharge the control  
10 surface and cantilever beam with opposite polarity and delay the full reduction of the coulomb force. The speed at which this discharge mechanism can operate is determined by the complex impedance of the control surface current path, the cantilever beam current path (which is the other side of the capacitor storing the surface charges) and the external circuit for the control signal.

15 The method of the above-referenced Streeter application speeds the time required to open a MEM switch constructed in accordance with the teachings provided herein. The inventive switch provides a coulomb repulsion force which assists the cantilever spring force in opening the switch. The two forces act in the same direction and are additive. The teachings of the above-referenced Streeter application may allow  
20 for switch opening to occur over a shorter time span than is required to close the MEM switch. The opposite condition often occurs in conventional MEM switches. Whereas the conventional MEM switch has only the "pull" closing electrostatic force, the improved switch structure of the above-referenced Streeter application has a "push" operation by which an electrostatic coulomb force aids in opening the switch.

25 Fig. 5 is a diagram of an improved MEM switch constructed in accordance with the teachings of the above-referenced Streeter application. As shown in Fig. 5, the improved switch 10 includes an insulating substrate 12, a conductive contact 14, a cantilever support 16, a first conductive surface 18 and a cantilever beam 20 as per the conventional switch 10' of Fig. 1. However, in accordance with the present teachings,

a first control surface 30 is provided on the lower surface 31 of the beam 20. The first control surface 30 is insulated from the beam 20 by a layer of insulation 32. A second control surface 34 is disposed over the first conductive surface 18 and is separated therefrom by a layer of insulative material 36.

5           The physical improvements illustrated in Fig. 5 over the conventional MEM switch structure illustrated in Fig. 1 are the charge storage structure on the cantilever beam 20 (consisting of the conductive beam 20, the first control surface 30 and the dielectric insulator 32 therebetween) and the addition of a charge storage structure (consisting of the first conductive surface 18, the second control surface 34 and the  
10           insulator 36 therebetween) as a replacement to the conductive control surface of the conventional MEM switch of Fig. 1. The two charge storage additions are used to induce the equal and like polarity charges that will result in a repulsive coulomb force during the opening process as discussed more fully below. The inventive structure allows for the creation of coulomb forces of either attraction or repulsion as will be appreciated by those skilled in the art. The continuous mechanical connection between  
15           the cantilever beam, the cantilever support, the first conductive surface 18 and the support substrate allows the coulomb forces to be properly placed on the cantilever beam.

          Those skilled in the art will also recognize that the teachings of the above-  
20           referenced Streeter application may be realized in additional structural designs that allow one to create two controllable charge storage areas capable of exerting both attractive and repulsive coulomb forces on the cantilever beam. In addition, in certain applications, i.e., optical, the first control surface 30 and insulation 32 may not be required. The first control surface 30 serves to facilitate the electrostatic repulsive  
25           force on the beam 20 while isolating the electrical circuit to which the beam 20 is connected on closure of the switch 10.

          A variable capacitor is formed by the two control surfaces 30 and 34 and the dielectric (air, vacuum, inert gas, etc.) therebetween. This capacitor must be considered in addition to the two fixed capacitors (34, 36, 18) and (30, 32, 20) formed

by the control surfaces mentioned above. The variable capacitance is minimum when the switch is open and is maximum when the switch is closed.

The closing process for the improved MEM switch 10 is the same as that of the conventional MEM switch 10'. Opposite polarity charges are induced on the first and second control surfaces. The opposite charges create an attractive coulomb force as discussed above. These forces must overcome the cantilever spring restorative force, and there is a minimum charge that allows switch closure. There is also a maximum charge and associated voltage that can be tolerated as discussed above.

Fig. 6 is a schematic diagram of an electrical circuit using the improved MEM switch of the above-referenced Streeter application. Those skilled in the art will appreciate that numerous circuit configurations are permitted using the improved MEM switch of the above-referenced Streeter application. In Fig. 6, a first control voltage supply 21 provides a control voltage  $V_{c1}$  to the first control surface 30 on the cantilever beam 20 and a second control voltage supply 22 provides a second control voltage  $V_{c2}$  to the second control surface 34. Note the depiction of the equivalent capacitors C1, C2 and C3 representing the fixed capacitor provided by the first control surface 30 and the beam 20, the second control surface 34 and first conductive area 18, and the variable capacitance between the first and second control surfaces 30 and 34, respectively. Charging the control surfaces may be considered to be equivalent to charging the capacitors C1, C2 and C3. The closure speed depends on the time it takes to charge these capacitors. In all probability, equivalent capacitors C1 and C2 will dominate the charging process. Low impedance circuits are required to minimize the charging time of capacitors C1 and C2.

Opposite charges can be induced on the two control surfaces by applying opposite voltage polarities to the two control surfaces as connected in Figure 6. While the maximum attractive force will result from having the two charges on capacitors C1 and C2 equal and opposite, there need not be charge equality on the two control surfaces. Further, there need not be a specific voltage polarity on the first or

the second control surface. Nonetheless, a specific implementation may favor a defined polarity structure or a continuous variation of polarity in the driving signals.

As discussed above with respect to the conventional MEM switch of Fig. 2, the application of a fixed direct current (D.C.) voltages  $V_{c1}$  and  $V_{c2}$  to the control surfaces 30 and 34 of the improved MEM switch 10 of the above-referenced Streeter application is the simple case of the control waveform driving the MEM switch 10 to the closed position. The voltage  $V_c$  may be of either polarity, although the physical structure and the materials used in fabrication of the MEM switch may favor one polarity over the other. The application of the voltage to the control surfaces 30 and 34 will cause a charging current to flow briefly in the control circuit (consisting of the first and second control surfaces 30 and 34 and the first and second control voltage supplies 21 and 22). This charging current can be thought of as charging the capacitor C3 formed by the first and second control surfaces 30 and 34, respectively. The difference in potential between the control voltages  $V_{c1}$  and  $V_{c2}$  must be above the minimum and below the maximum, for the physical structure of the MEM switch, if proper operation is to occur. This minimum voltage and charge is dependent on the physical parameters of the switch and variations in the fabrication process. It is normally determined experimentally for each and every switch. Typical values are 5V to 50V. Similarly, the maximum voltage and charge is discussed on page 6 line 20, 21,22, and elsewhere in the discussion. It is also determined experimentally,

As per the conventional MEM switch 10' of Fig. 1, the speed of closure of the switch 10 can be controlled to some degree by controlling the magnitude of the charges on the control surfaces. The initial charges placed on the control surfaces will have a maximum value set primarily by arc limitations between the control surfaces and the remaining elements of the MEM switch. This maximum charge will apply a maximum coulomb force to the cantilever beam, resulting in a maximum initial closure rate for the beam. As the beam approaches the control surface during closure, the capacitance will increase. While application of a constant voltage will result in an increase in the surface charge (through  $Q=CV$ ) and a resultant increase in the coulomb

force beyond the square-law effect, the voltage may exceed the capabilities of the beam to control surface spacing. Thus, it may be necessary to reduce the control voltage as the switch closes to prevent a discharge arc of the stored charge. This leads to a decayed voltage wave shape versus time for the fastest MEM switch closure operation.

5 The shape of the control voltage decay for the fastest closure depends on the constructional details of the MEM switch 10. When the MEM switch achieves closure, the control voltage must remain between the maximum closed voltage (determined by arc or cantilever deflection) and the minimum voltage needed to provide sufficient coulomb force needed to overcome the cantilever spring restoration

10 force. The optimum control voltage driving waveform for MEM switch closure depicted in Fig. 3 is applicable to the improved MEM switch 10 of the above-referenced Streeter application as well.

For the purposes of switch closure (only), it is possible to set the first control voltage,  $V_{c1}$ , equal to zero. This is equivalent to short circuiting capacitor C1. The

15 action of the charge distribution then becomes identical to the conventional MEM switch case, and second control voltage,  $V_{c2}$ , (relative to the rest of the MEM switch structure) determines the closure operation of the improved MEM switch 10. Setting the control voltage to zero also has the secondary benefit of causing the first control surface 32 to act as an electrostatic shield for the cantilever beam 20. This may be

20 useful in low level signal applications where the control signal could be considered as a potential source of interference to the switched signal.

It is also possible to reverse the above case, and set the second control voltage  $V_{c2}$ , equal to zero. This is a mode that is available only in the improved MEM switch 10 of the above-referenced Streeter application. The operation is otherwise identical

25 to the conventional case. The electrostatic shield offered by the first control surface 30 is no longer applicable for this case.

The MEM switch is held in the closed position by a continuous application of the electrostatic attraction force. This usually means maintaining the control voltages

$V_{c1}$  and  $V_{c2}$  for the duration of the closure time, thus maintaining the charges on the control surfaces responsible for the coulomb attractive force.

There are a large variety of values and waveforms for the first and second control voltages  $V_{c1}$  and  $V_{c2}$  that will cause the MEM switch 10 to close. Fig. 7 depicts one of the many possible drive waveforms for the improved MEM switch 10 of the above-referenced Streeter application. In Fig. 7, both the closing and opening process waveforms are shown.

The process for opening the improved MEM switch of the above-referenced Streeter application is as follows. The control voltages  $V_{c1}$  and  $V_{c2}$  are applied to the first and second control surfaces 30 and 34 respectively and are set equal and non-zero to create a repulsion electrostatic charge that aids in opening the switch. In the conventional MEM switch 10' the control voltage is just set to zero to remove the electrostatic charge. In the simplest configuration, either  $V_{c1}$  or  $V_{c2}$  is reversed in polarity with respect to the control voltages used to close the improved MEM switch 10. This places charges of the same polarity on the two control surfaces 30 and 34, and creates a repulsion electrostatic coulomb force pushing the cantilever beam away from the conductive contact.

This repulsion force adds directly to the spring restorative force of the cantilever beam 20 and pushes the cantilever beam away from the contact 14 more rapidly than the spring restorative force alone. Depending on the design configuration of the MEM switch 10, the repulsion force can be significantly larger than the spring restorative force, resulting in a switch design that is significantly more resistant to contact "stiction" problems and which opens very rapidly.

With respect to the need to avoid excess voltage to prevent arcing, it should be noted that in the process of opening the improved MEM switch, there cannot be an arc between the two control surfaces if they are at the same or nearly the same potential and polarity. Thus, the opening voltage is limited by the arc voltage to other structures of the MEM switch 10 rather than between the control surfaces as was noted for the conventional MEM switch 10'.



Fig. 7 provides an example of the control waveforms appropriate to open MEM switch of Streeter *et al.*. The waveforms shown are two of a variety of waveforms that are possible within the scope of the present teachings. Some broad limitations can be placed on the waveforms as shown. The voltages "Max  $V_c$ " and "End  $V_c$ " of either polarity must not result in arcing to any element of the MEM switch 10. During the closing operation as shown, control voltages  $V_{c1}$  and  $V_{c2}$  must be of opposite polarity. Optimum attraction coulomb force will result if the two voltages  $V_{c1}$  and  $V_{c2}$  are maximum, equal, and opposite polarity. During the opening operation, control voltages 1 and 2 must be the same polarity. Optimum repulsion force will exist if the two voltages are maximum, equal, and the same polarity. The start and end of the closure and opening process are indicated in the figure.

Although Fig. 7 shows D.C. (direct current) voltages as the driving waveform, A.C. (alternating current) voltages may also be used. The use of A.C. driving voltages will cause a constant charging, discharging, and opposite polarity recharging of the equivalent capacitors C1, C2, and C3. A.C. waveforms may be useful in combating dielectric polarization that reduces the coulomb force available. The driving waveforms should always hold the correct polarity structure on control surfaces 30 and 34.

Fig. 7 also shows an optional discharge operation following the switch opening process. The purpose of this discharge operation is to remove the electrostatic coulomb repulsive force applied to the cantilever beam when it is in the open position. If the coulomb force remains applied to the beam 20, the cantilever beam will be pushed past the open rest position (the neutral force open position) to a position of greater opening. The greater opening will enhance the voltage that the switch can withstand when open. It will also increase the cantilever spacing from the control surface attached to the substrate and the spacing to the conductive contact. The increased spacing will result in greater signal path isolation and a reduced initial coulomb attractive force during the closing process. The increased spacing will also force a longer time for the switch to close. The increased closing time is somewhat

compensated by the cantilever spring restorative force pushing the beam back to the neutral open position. There exists a trade-off between the switch closure time and the switch open standoff voltage rating (and isolation) as a result of the coulomb repulsive force available in the improved MEM switch 10.

5           Although a linear discharge waveform is shown in Fig. 7, any appropriate means of discharge may be used. Generally, it may be optimum to allow the charges on each control surface to decay in the same proportion as a function of time. This will result in a reduction in the magnitude of the coulomb force without encountering secondary effects that may result from discharging the two control surfaces in unequal  
10   time frames.

Fig. 3 previously presented an optional waveform to enhance the speed of closure by utilizing a higher initial voltage at the start of the closing operation, and reducing the voltage as the closing operation progresses to an end closure voltage. That waveform is also shown in Fig. 7 on control voltage  $V_{c1}$ . Control voltage  $V_{c2}$  is  
15   shown with an optional waveform that is constant during closure. Either waveform can be used in any combination desired for control voltages  $V_{c1}$  and  $V_{c2}$ . There are other waveforms also acceptable for switch closure, including the previously mentioned A.C. waveforms. If the waveforms of control voltages  $V_{c1}$  and  $V_{c2}$  both contain the increased initial voltage (+Max  $V_c$  and -Max  $V_c$  at the start of closure) the  
20   limitation against arcing must continue to apply.

The opening operation can potentially benefit from the same increased voltage in the case of the improved MEM switch 10. The use of the increased voltage is shown on control voltage  $V_{c1}$ , but it may also be used on control voltage  $V_{c2}$  if desired, subject to the limitation on arcing to other structures in the MEM switch. As shown,  
25   control voltage  $V_{c2}$  uses a constant voltage during the opening operation, and this voltage is equal to the voltage used to close the switch. Control voltage  $V_{c1}$  starts the opening process at the "end  $V_c$ " voltage of the closing operation. As the charge on the equivalent capacitor  $C1$  is reversed, the voltage may be (rapidly) increased to the arc-limited value "Max  $V_c$ ". As the cantilever beam 20 draws away from the

conductive contact 14, the spacing between the two control surfaces 30 and 34 will increase. Since the two control surfaces 30 and 34 are now at the same polarity, the maximum voltage is now determined by arc limitations to other MEM switch structures. The shape of the voltage increase is bounded by the arc voltage, and for example may be determined by the discharge and opposite polarity recharge between the two control surfaces 30 and 34.

Fig. 7 also assumes that the maximum allowable voltage on the first control surface 30 is "+Max Vc" or "-Max Vc", which defines the voltage peak values shown in Fig. 7.

Fig. 8 is a diagram of the single pole, double throw MEM switch of the present invention. The inventive switch 100 is essentially identical to that disclosed in Fig. 5 above with the exception that second conductive contact 115 is added on the insulating support substrate 112. In operation, the repulsive coulomb opening force pushes the cantilever beam into contact with the second conductive contact 115. The attractive coulomb force disconnects the second contact 115 and pulls the cantilever beam 120 into contact with the first contact 114.

A possible disadvantage of the switch 100 of Fig. 8 is that the coulomb force is inversely proportional to the square of the separation between first and second control surfaces 130 and 134 respectively. While there are large coulomb forces involved in closing and opening the switch 100 with respect to the first contact 114, the coulomb forces are weaker in opening and closure with respect to the second contact 115. It is likely that the second conductive contact 115 would have to be located very close to the rest position of the cantilever beam 120 and that it would be difficult to exert significant contact pressure to hold the cantilever beam 120 against second conductive contact 115.

Fig. 9 is a diagram of an alternative embodiment of the single pole, double throw MEM switch of the present invention without isolation between the switched signal and the control signal. In this embodiment, the switch 200 has a first insulating substrate 212 on which a first conductive contact 214, a first control surface 234 and a

bottom cantilever beam support 216 are mounted. A conductive, flexible cantilever beam 220 is suspended at one end thereof between the bottom cantilever support 216 and a top cantilever beam support 217. A second insulating support substrate 213 is mounted on the top cantilever beam support 217. A second conductive contact 215  
5 and a second conductive control surface 230 are mounted under the second insulating support substrate 213. The switch 200 provides for attractive coulomb forces to close either contact. Contact opening forces are supplied by the spring restorative force of the cantilever beam 220.

In operation, either the first or the second control surface 230 or 234 is  
10 charged. The opposite control surface must be discharged to provide a minimum of undesired coulomb force from the opposite direction. With neither control surface charged, the cantilever beam 220 hangs midway between the two conductive contacts 214 and 215. The switch 200 has three stable states, with both contacts open and no applied charge, or with one of the two conductive contacts being in physical contact  
15 with the cantilever beam 220 when the associated control surface is charged. The tri-state functionality of this switch configuration is not available in conventional mechanical switches, although it may be available in solid state semiconductor bus driver devices.

The switch 200 may be fabricated in subassemblies (the base, the cantilever  
20 beam structure, and the top) which are assembled into the complete switch as shown. Although shown in one physical layout (vertical), the switch 200 can have any orientation without departing from the scope of the present teachings.

Fig. 10 is a diagram of a second alternative embodiment of the single pole, double throw MEM switch of the present invention with isolation between the  
25 switched signal and the control signal. Fig. 10 is the extension of the speed enhanced version of the MEM switch in Fig. 9. The embodiment 300 of Fig. 10 combines the teachings of Figs. 5 and 9 and includes a supplemental conductor 338 disposed beneath a second insulating layer 338. An insulating layer 342 is sandwiched between the

supplemental conductor 318 and a third control surface 340. A second insulating layer 346 is sandwiched between a fourth control surface 344 and the beam 320.

Separate top and bottom control surfaces provide the capability to use separate driving functions for the top and bottom switch structures. This allow for simultaneous  
5 push and pull operation for enhanced speed.

Placing the cantilever beam conductive control surfaces 330 & 344 of Fig. 10 at the ground common potential provides an electrostatic shield between the signal currents on the cantilever beam and the control signals providing the coulomb forces. This structure thus provides signal isolation enhancement when compared to simpler  
10 cantilever beam structures.

The circuitry of Fig. 6 would be duplicated for each of the switch positions to operate with the switch of Fig. 10 of this disclosure. This doubles the number of control voltage sources.

Thus, the present invention has been described herein with reference to a  
15 particular embodiment for a particular application. Those having ordinary skill in the art and access to the present teachings will recognize additional modifications applications and embodiments within the scope thereof.

It is therefore intended by the appended claims to cover any and all such applications, modifications and embodiments within the scope of the present invention.

20 Accordingly,

WHAT IS CLAIMED IS:

## CLAIMS

1. A single pole, double throw electrostatically actuated micro-electromechanical switch comprising:
  - a first contact providing a first terminal of said switch;
  - a second contact providing a second terminal of said switch;
  - 5 a cantilever beam providing a third terminal of said switch; and
  - a mechanism for electrostatically pushing said beam to disengage said first contact and engage said second contact.
2. The invention of Claim 1 wherein said system for electrostatically pushing said switch includes a first charge storage structure on said beam, a second charge storage structure, and an electrical supply for creating an electrical charge on said first and said second charge storage structures, said first and said second charge storage  
5 structures being effective to create a force of repulsion therebetween on the application of an electrical charge thereto having a first polarity by said supply.
3. The invention of Claim 1 wherein said first and said second charge storage structures are effective to create a force of attraction therebetween on the application of an electrical charge thereto having a second polarity by said supply.
4. The invention of Claim 1 further including a third charge storage structure for pushing said beam to disengage said second contact and to engage said first contact.
5. The invention of Claim 4 further including means for electrostatically pushing and pulling said beam simultaneously in the same direction.

6. A switching method including the steps of:
- electrically connecting a first contact to a first terminal of said switch;
  - electrically connecting a second contact to a second terminal of said switch;
  - electrically connecting a throw to a third terminal of said switch; and
- 5        electrostatically pushing and/or pulling said throw to disengage said first contact and engage said second contact.

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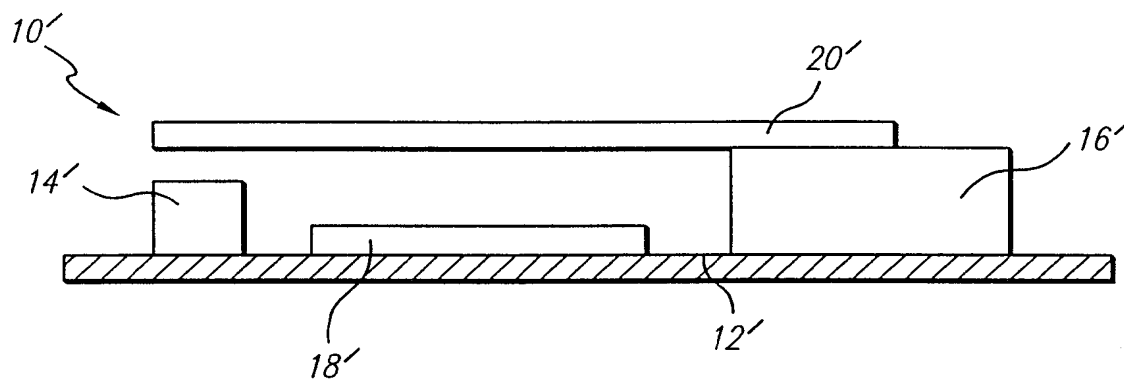


FIG. 1

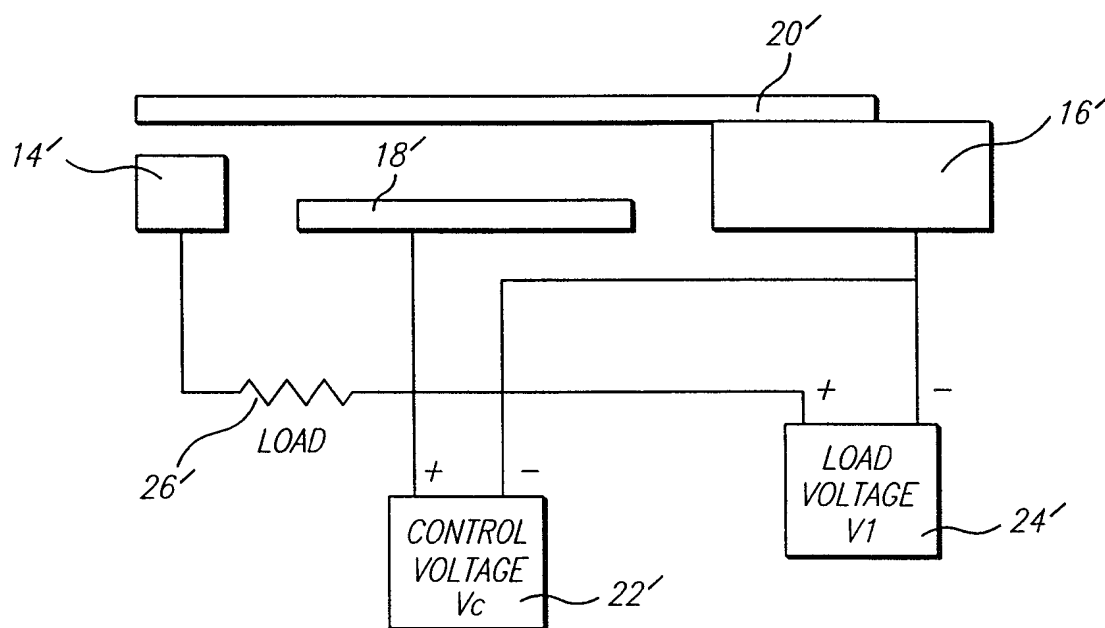


FIG. 2



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FIG. 3

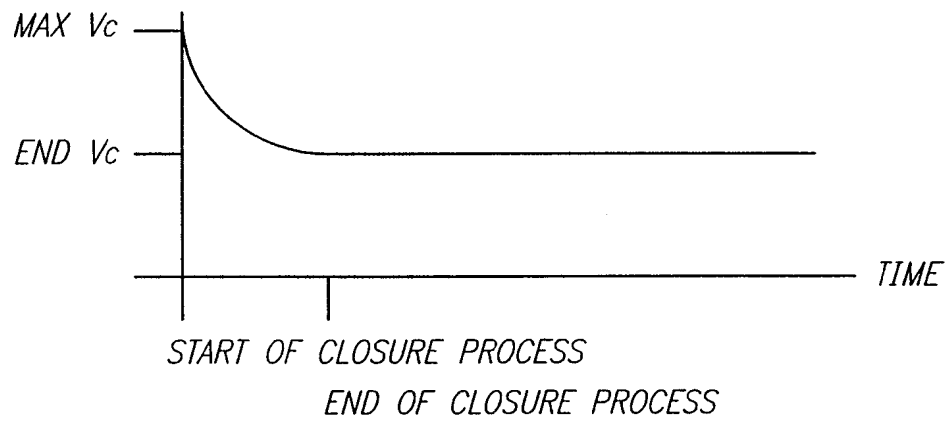
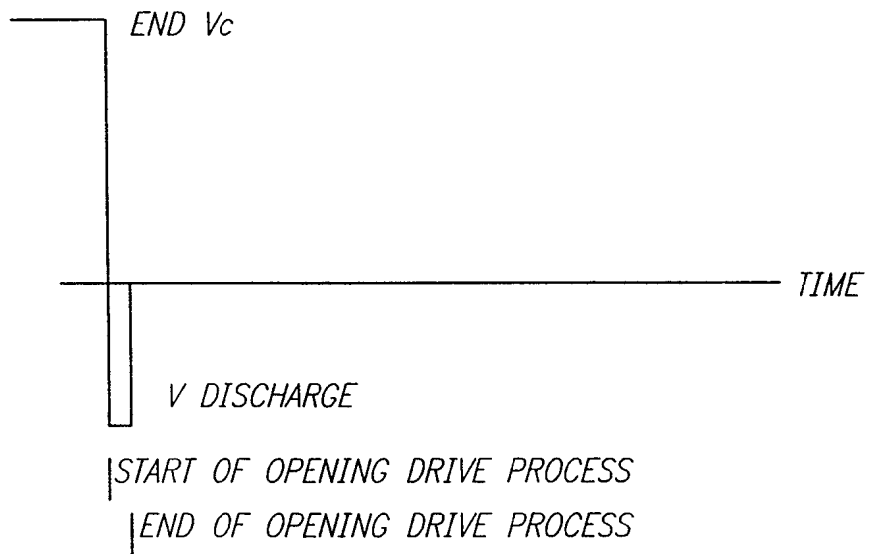


FIG. 4



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FIG. 5

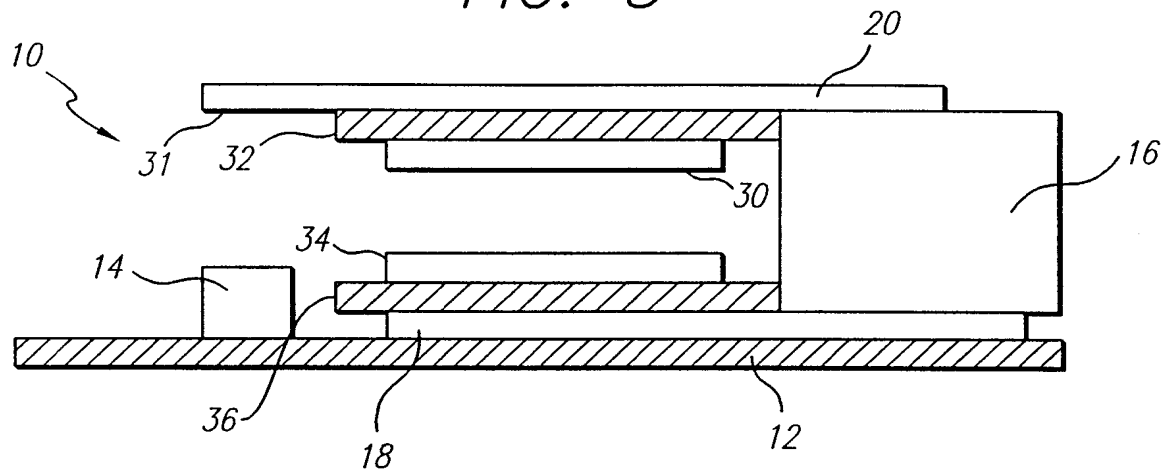


FIG. 6

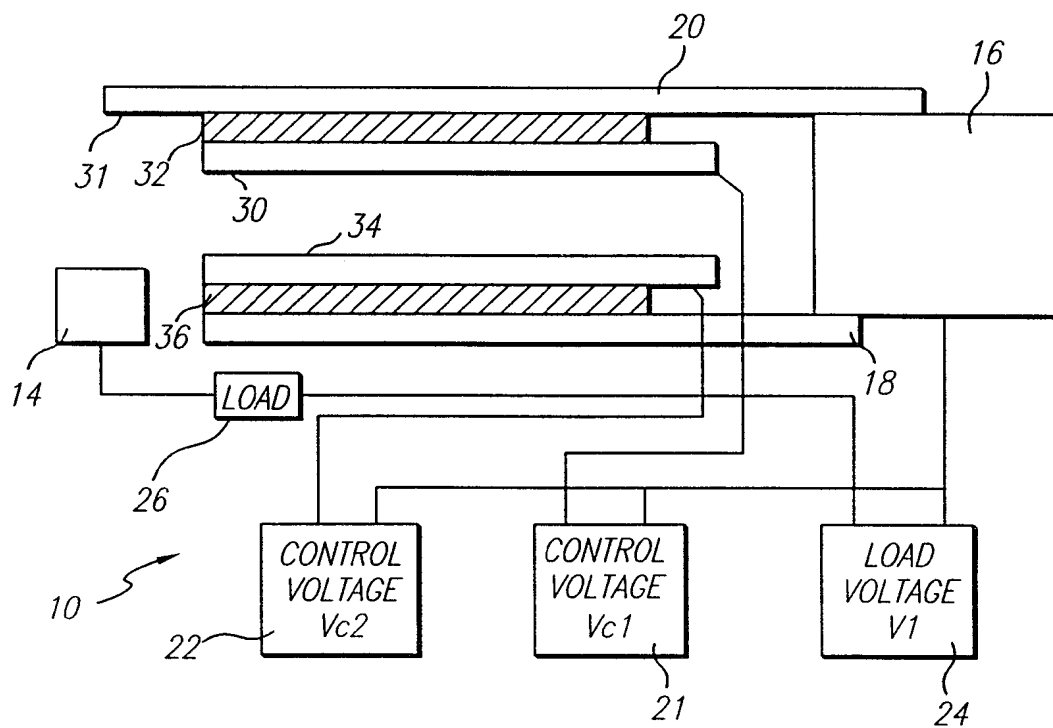
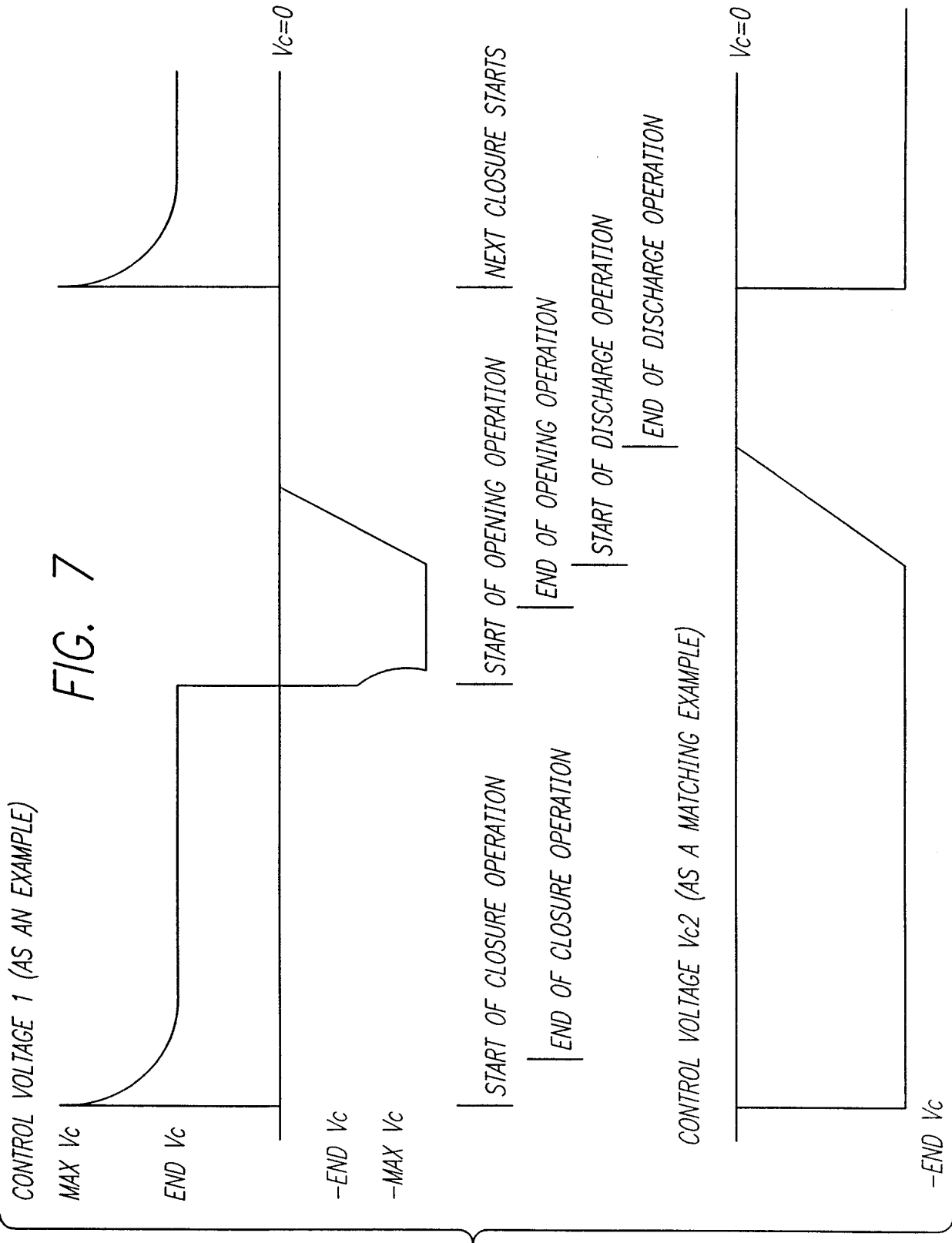


FIG. 7



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FIG. 8

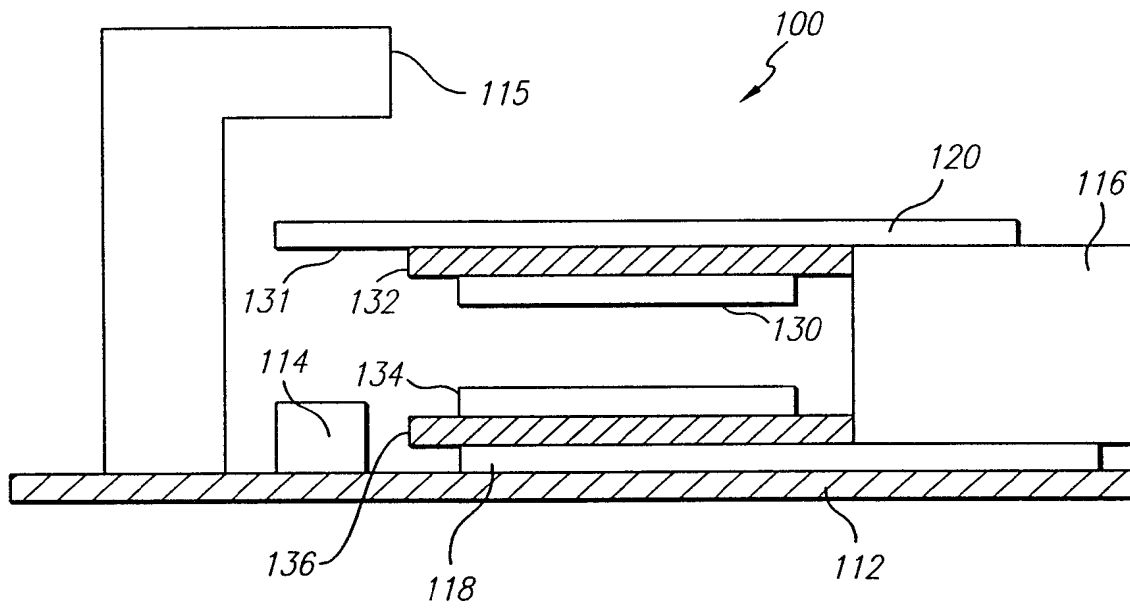
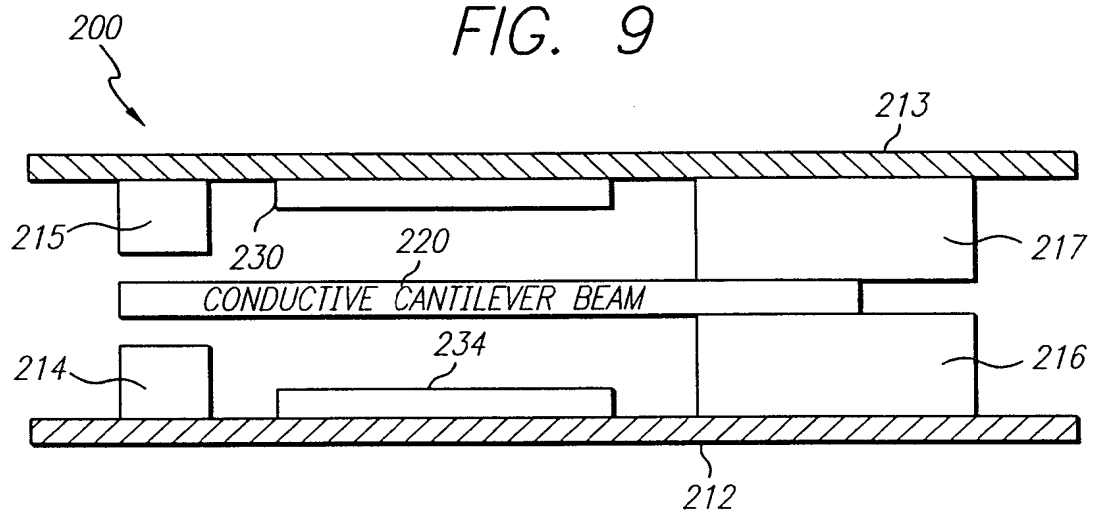
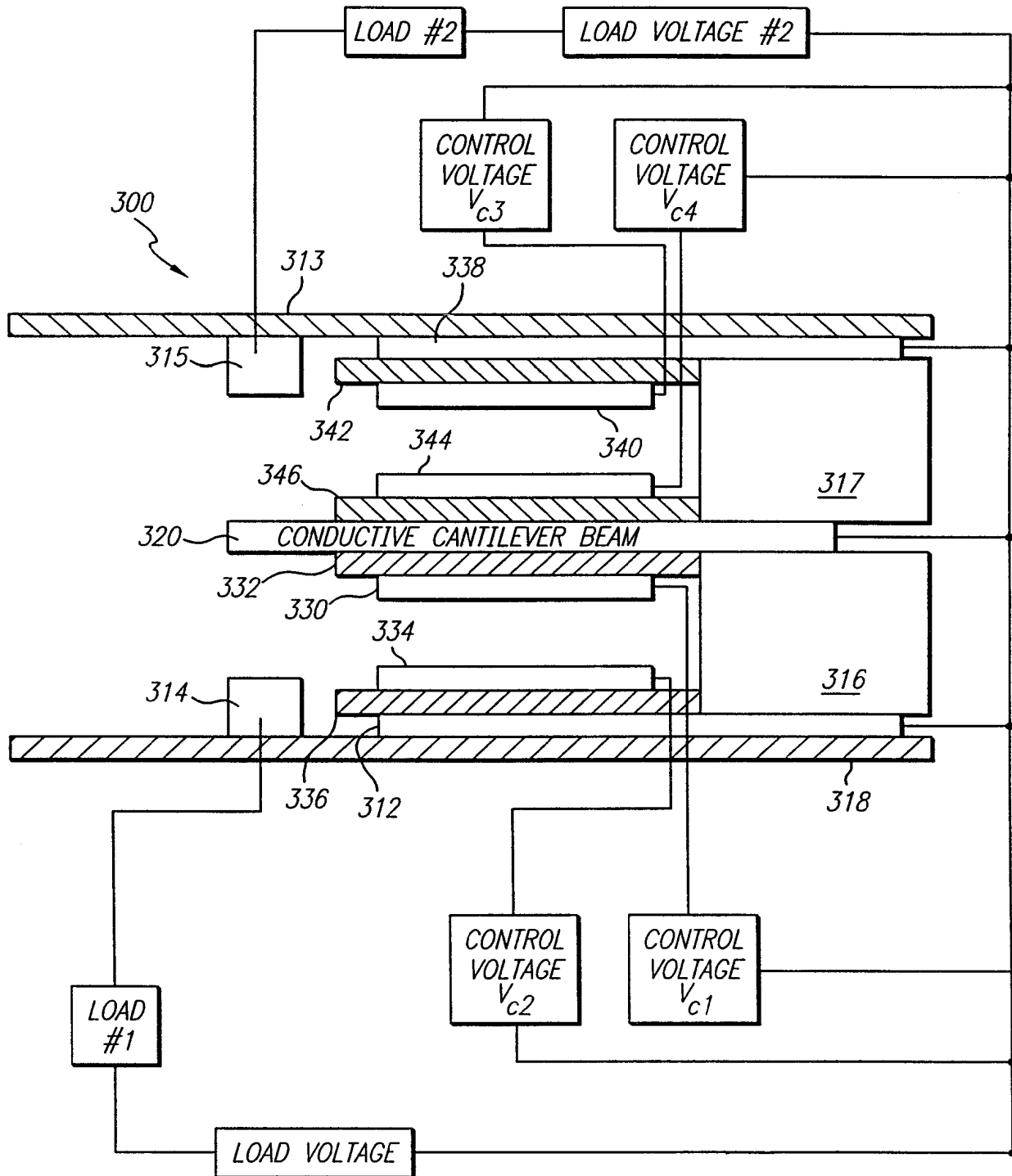


FIG. 9



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FIG. 10



# INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 00/05176

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 H01H59/00

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 H01H

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

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A	EP 0 608 816 A (DIDIER PERINO ;LEWINER JACQUES (FR); MATSUSHITA ELECTRIC WORKS LTD) 3 August 1994 (1994-08-03) abstract; claims; figures	1-6
A	EP 0 892 419 A (TRW INC) 20 January 1999 (1999-01-20) abstract; claims; figures	1-6
A	DE 42 05 029 C (SIEMENS) 11 February 1993 (1993-02-11) claims; figures	1-6
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☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

3 July 2000

Date of mailing of the international search report

10/07/2000

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# INTERNATIONAL SEARCH REPORT

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## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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